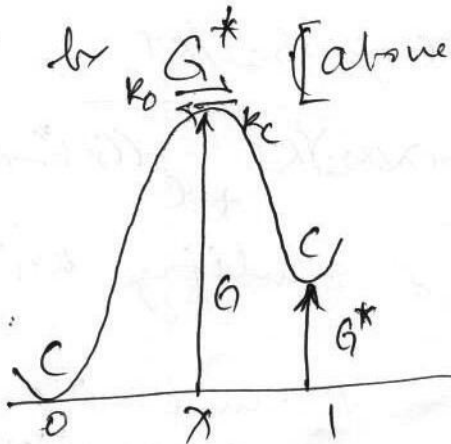


# ASSIGNMENT - I

## PROBLEM - 1

Let the free energy change needed at the barrier be  $G$  at location  $\lambda$  in moving from closed (C) at 0 to open (O) state at 1. Let the energy in open state be  $G^*$  [above (C)].



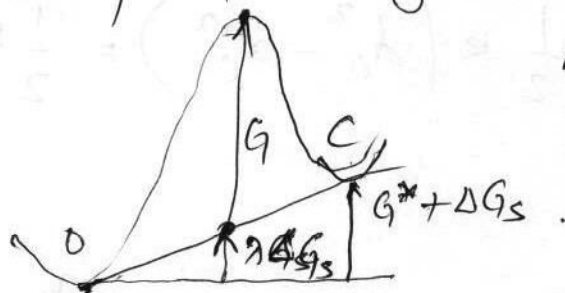
If  $d_c$  and  $d_o$  are lengths of the spring with channel closed and channel open respectively.

⊗

Thus change in potential energy when channel opens =  $\Delta G_s = \int_{d_c}^{d_o} kx dx$

$$= \frac{k}{2} (d_o^2 - d_c^2)$$

Thus the barrier is modified by ramp of height  $\Delta G_s$ .



$$k_c = \alpha e^{-(G-G^*-\Delta G_s)/RT}$$

$$k_o = \alpha e^{-(G+\lambda\Delta G_s)/RT}$$

Rate of channel opening

$$\frac{dO}{dt} = -k_c O + k_o C = -k_c O + k_o (T - O)$$

where T is the total conc. of channels.

$$\Rightarrow \frac{dO}{dt} = k_0 T - (k_0 + k_c) O$$

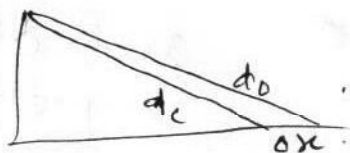
At steady state  $\frac{dO}{dt} = 0$

Probability of open channel,

$$= \frac{O}{T} = \frac{k_0}{k_0 + k_c}$$

$$= \frac{e^{-(G + \lambda \Delta G_s)/RT}}{e^{-(G + \lambda \Delta G_s)/RT} + e^{-(G - G^* - \Delta G_s)/RT}}$$

Take  $\lambda = 1/2$  and simplify with  $\Delta G_s = \frac{1}{2}k(d_0^2 - d_c^2)$



Assume  $\Delta x$  the separation is very small.

$$d_c = \sqrt{x^2 + y^2}$$

$$d_0 = \sqrt{(x + \Delta x)^2 + y^2}$$

$$= \sqrt{x^2 + y^2 + 2x\Delta x + \Delta x^2}$$

using  $\Delta x$  very small.

$$d_0 \approx d_c + \frac{x\Delta x}{d_c}$$

$$\Delta G_s = \frac{1}{2}k(d_0^2 - d_c^2) = \frac{1}{2}k \left[ \left( d_c + \frac{x\Delta x}{d_c} \right)^2 - d_c^2 \right]$$

$$= \frac{1}{2}k \left[ d_c^2 + 2x\Delta x + \frac{x^2\Delta x^2}{d_c^2} - d_c^2 \right]$$

$$\approx kx\Delta x$$

Substitute in  $\frac{O}{T} \approx kx\Delta x$

From above the rate constants are a function of separation  $x$ .

$$\frac{dO}{dt} = k_o(x_1)T - [k_o(x_1) + k_c(x_1)]O$$

When set apart to  $x_1$ ,  
 at  $t = 0^+$  the  $O$  value is  
 $T \frac{k_o(x_0)}{k_o(x_0) + k_c(x_0)}$ . When held  
 at  $x_0$  for  
 long.

Thus

$$\frac{dO}{dt} = T \left[ \frac{k_o(x_1)}{k_o(x_1) + k_c(x_1)} - [k_o(x_1) + k_c(x_1)] \frac{k_o(x_0)}{k_o(x_0) + k_c(x_0)} \right]$$

Rate of opening of channels.

### PROBLEM - 2.

if before an <sup>change in voltage</sup> clamp, the voltage is held steady at  $V_1$  and it is changed to  $V_2$

then

$$\frac{dh}{dt} = \frac{h_{\infty}(V_2) - h}{\tau_H(V_2)}$$

describes the change in  $h$ .

with  $h(0) = h_{\infty}(V_1)$

The solution to the above diff. eqn.

$$h(t) = h_{\infty}(V_2) + [h_{\infty}(V_1) - h_{\infty}(V_2)] e^{-t/\tau_H}$$

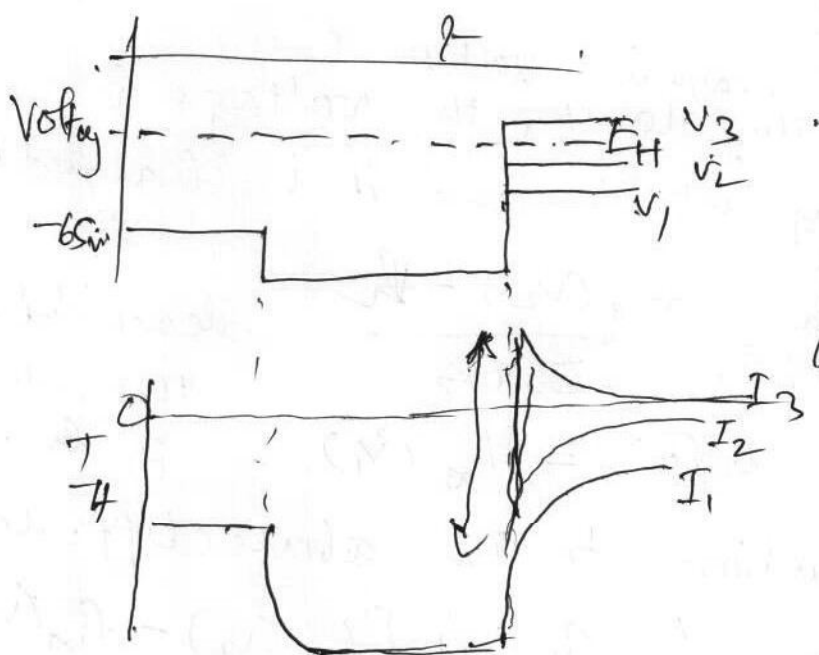
$h$  ~~increases~~ changes exponentially from

$$h_{\infty}(V_1) \text{ to } h_{\infty}(V_2)$$

$$\tau_H(t) = \frac{1}{g_{H+}} [h_{\infty}(V_2) + [h_{\infty}(V_1) - h_{\infty}(V_2)] e^{-t/\tau_H}]^{-1} \cdot (\bar{V}_2 - E_H)$$

$E_H = -43 \text{ mV}$ . All the clamp potentials used are below  $E_H$ . Thus all the currents are inward currents & only increase or decrease from the holding current which is a high inward -ve current at the initial position of the clamp. So there is no "actual" reversal in polarity.

To determine  $E_H$ ,  $I_H$  must go to zero from 0 current. Thus a clamp protocol where at the tail the clamp potential is changed to variety of values. like below.



where this true reversal would take place is  $E_H$ .

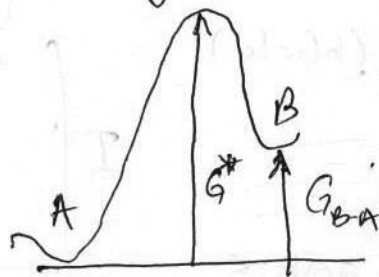
Determining  $I_H$  (nA) &  $E_H$  (mV) was discussed in class. (like other HH gating variables).

# PROBLEM - 3

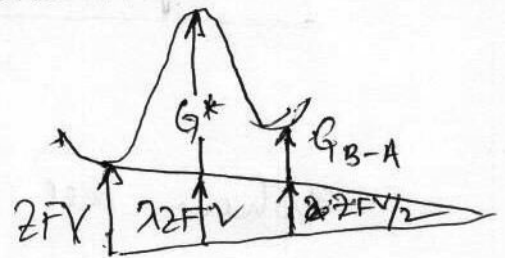
In the top model. the binding of  $Z^{2+}$  to the channel is not affected by the transmembrane potential. because the ~~the~~ ligand (ion)  $Z^{2+}$  does not move through any fraction of the membrane. Whereas in the second case the  $Z^{2+}$  ion goes through half of the membrane potential's field to the binding site.

A is  $Z^{2+}$  unbound to channel state & B is  $Z^{2+}$  bound to channel state. the following barrier diagrams are appropriate.

Top case



If  $V$  is the membrane potential.  $V_{in} - V_{out}$



Problem 4 (Part A discussed in class)

Problem 4 (Part B)

$$I_{ext} = C \frac{dV}{dt} + \bar{g}_K n^4 (V - E_K) + \bar{g}_L (V - E_L) \quad \text{--- (1)}$$

$$\frac{dn}{dt} = \alpha(V)(1-n) - \beta(V)n$$

Small signal deviation

$$I_{ext} = I_{ext}^r + i_{ext} \quad V = V^r + v \quad n = n^r + \eta$$

$\alpha(V)$  &  $\beta(V)$  linearized functions of  $v$

$$\alpha(V) = \alpha^r + a v \quad \beta(V) = \beta^r + b v$$

Substituting the above in (1)

$$\text{(2) ... } \left[ \begin{aligned} I_{ext}^r + i_{ext} &= C \frac{d(V^r + v)}{dt} + \bar{g}_K (n^r + \eta)^4 (V^r + v - E_K) \\ &\quad + \bar{g}_L (V^r + v - E_L) \\ \frac{d(n^r + \eta)}{dt} &= (\alpha^r + a v)(1 - n^r - \eta) - (\beta^r + b v)(n^r + \eta) \end{aligned} \right.$$

Now  $(n^r + \eta)^4 \approx n^{r4} + 4n^{r3}\eta$  (neglecting higher powers of  $\eta$ )

at  $V^r$   $\frac{dV}{dt} = 0$  &  $\frac{dn}{dt} = 0$

Thus  $I_{ext}^r = \bar{g}_K n^{r4} (V^r - E_K) + \bar{g}_L (V^r - E_L)$

$\alpha^r (1 - n^r) - \beta^r n^r = 0$

Using the above in (2) and neglecting second and higher order terms of the small variables (also  $\eta^2$  etc.)

$$i_{ext} \approx C \frac{dv}{dt} + \bar{g}_K n^{r4} v + 4\bar{g}_K n^{r3} \eta (V^r - E_K) + \bar{g}_L v$$

$$\frac{d\eta}{dt} \approx -\alpha^r \eta + a(1 - n^r)v - \beta^r \eta - b n^r v$$



PROBLEM 5

$$\frac{du}{dt} = 1 - (b+1)u + au^2v$$

$$\frac{dv}{dt} = bu - au^2v$$

Eq pts are intersection of nullclines.

$$\frac{du}{dt} = 0 \Rightarrow v_{unc} = -\frac{1-(b+1)u}{au^2} \quad \left. \begin{array}{l} \text{for } \\ u \neq 0 \end{array} \right\}$$

$$\frac{dv}{dt} = 0 \Rightarrow v_{enc} = \frac{b}{au}$$

$$v_{unc} = v_{enc} \quad \text{for eq pt.}$$

$$\Rightarrow -\frac{1-(b+1)u}{au^2} = \frac{b}{au}$$

$$-1 + (b+1)u = bu$$

$$u_{eq} = 1 \quad v_{eq} = b/a \quad \left. \begin{array}{l} \text{eq.} \\ \text{pt.} \end{array} \right\}$$

$$J|_{eq} = \begin{bmatrix} -(b+1) + 2auv & au^2 \\ b - 2auv & -au^2 \end{bmatrix} \quad \left. \begin{array}{l} \text{at} \\ \text{eq pt} \end{array} \right\}$$

$$= \begin{bmatrix} b-1 & a \\ -b & -a \end{bmatrix}$$

For eigen values .

$$\det[\lambda I - J] = 0$$

$$\Rightarrow \lambda^2 + (a-b+1)\lambda + a = 0$$

$$\lambda = \frac{b-a-1}{2} \pm \frac{\sqrt{(b-a-1)^2 - 4a}}{2}$$

divide  
the term  
by (b-a-1)

$$\Rightarrow \lambda = \frac{b-a-1}{2} \left[ 1 \pm \sqrt{1 - \frac{4a}{(b-a-1)^2}} \right]$$

The eq pt. in the system would be spiral if

For that case  $\lambda$  is imaginary.

$$\frac{4a}{(b-a-1)^2} > 1 \Rightarrow a^2 - 2ab - 2a + 1 - 2b + b^2 < 0 \quad (1)$$

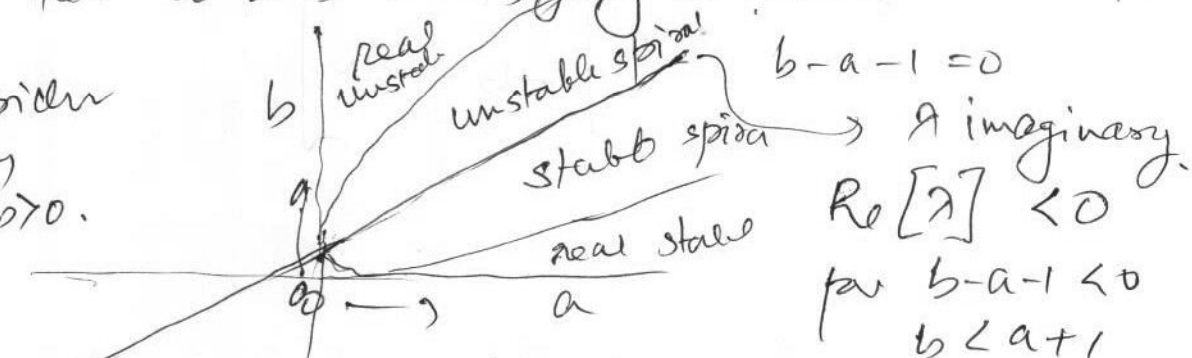
The boundary between real and complex regions in  $a$  &  $b$  - plane can be solved by setting (1) to 0. Also the form is symmetric in  $a$  &  $b$

the above gives  $a = (b+1) \pm 2\sqrt{b}$   
 $b = (a+1) \pm 2\sqrt{a}$

As  $a > 0$ ,  $b > 0$   
 real  $a \neq 0$   
 $b \neq 0$

For  $a$  &  $b$  satisfying the above

Consider only  $a > 0, b > 0$ .



Limit cycle cannot be proven. Why? Now consider for other 3 quadrants. (FOR YOU TO DO)